

Nuclear Fusion Power Reactor Concept Proposed for Laser-Driven Proton-Boron (HB11) Fusion

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First-Wall Life-Time Limitations and Solutions

HiPER technical report

- **1 Year from Neutron Radiation Damage** at Full 3GW-Fusion Radiation Power:
400MJ x 6.7Hz

- Solution: Increase First Wall
DISTANCE to Fusion Source: Reduce
Neutron Flux Increase Life-Time

- **~Seconds from Ion Radiation Damage =**
20% of Total Fusion Radiation Power for
DT

- Solution: Buffer Gas '**STOPS**' Ions:
Eliminates Damage see Book →

[2] R. Gonzales-Arrabal,

“Materials and Technology for Inertial Fusion
Reactors: Lessons Learned from the **HiPER**
Project”, DDFI-2025 .

[3] R. Gonzalez-Arrabal, A. Rivera, J.M.

Perlado,

“Limitations for tungsten as plasma facing material
in the diverse scenarios of the European inertial
confinement fusion facility HiPER: Current status
and new approaches”, Matter Radiat. Extremes 5,

Topical Nuclear Fusion HB11 Power Reactor –IWPBF-
055201 (2020)
Belgrade 08/09/2025

HiPER Building

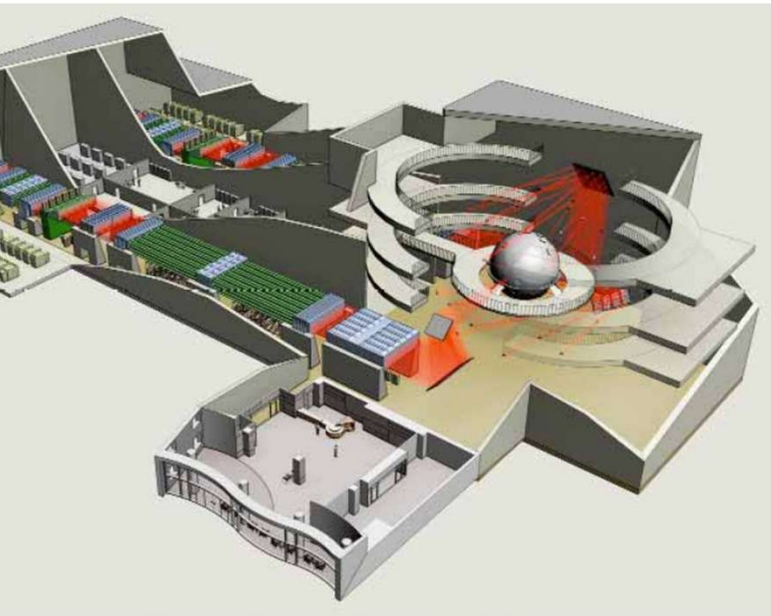
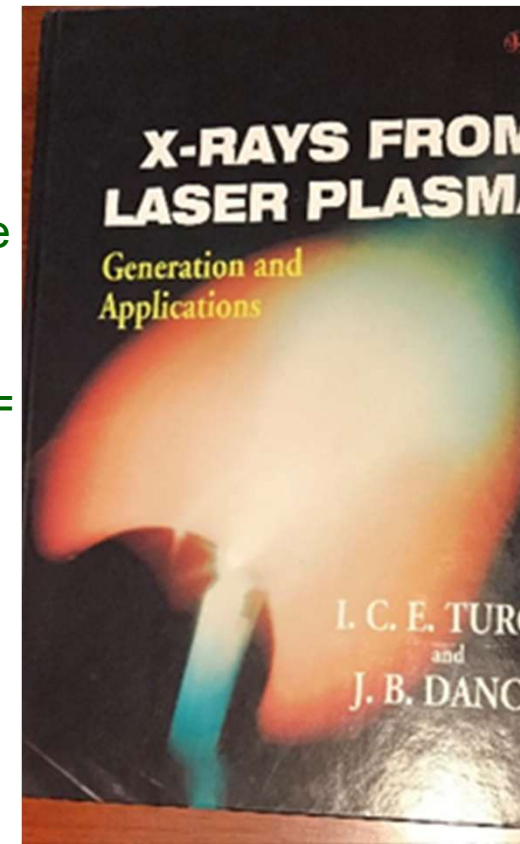


Figure 14.1 Aerial Schematic of HiPER

HiPER Technical Background
Conceptual Design Report 2007
Report is available on the HiPER website
hyper-laser.org



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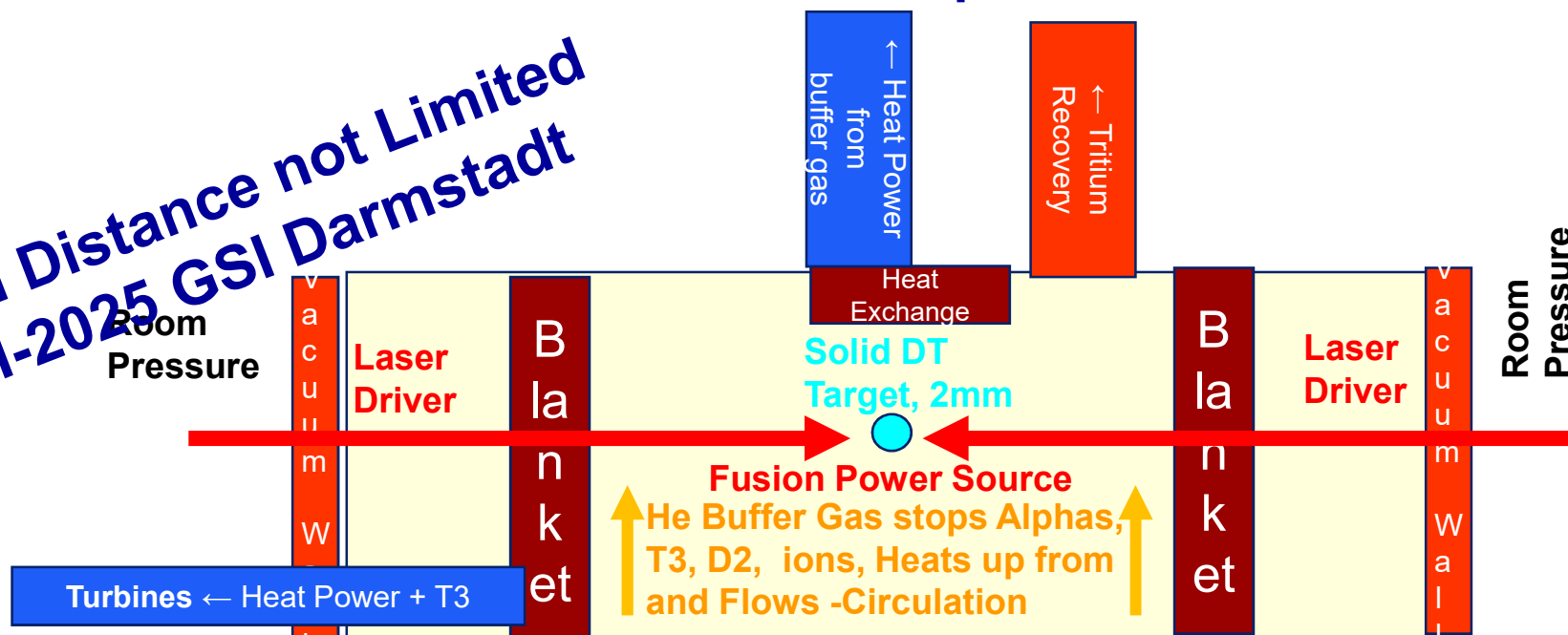


[4] ICE Turcu and Brian
“X-Rays from Laser Plasma
Generation and Applications
J Wiley and Sons, 1998

on Reactor Driven by Lasers: **No stringent space LIMITATIONS** on DIMENSIONS

Plasma/Reactor Chamber: Example for DT Reactor.

First Wall Distance not Limited
Diamond DDFI-2025 GSI Darmstadt



Laser Fusion Power (IFE) Reactor Proposal – schematic

- Small mm-size Solid DT target in Centre of Reactor
- Pulsed Operation – Scale Power by Laser Rep Rate

No stringent space LIMITATIONS on Plasma/Reactor Chamber DIMENSIONS

- Blanket Pannels, not Vacuum-tight convert 80% of P-Fusion + T3
- Blanket panels, and closest mirrors - consumables
- Vacuum wall separated in space from Blanket. Permanent wall.

Buffer Gas fills the whole Reactor/'Vacuum' Chamber

3MeV Alphas and Ion-debris stopped in Buffer Gas which heats up, converting 20% Fusion-Power to

Heat exchanger at top of Reactor sends this 20% Power to Turbines



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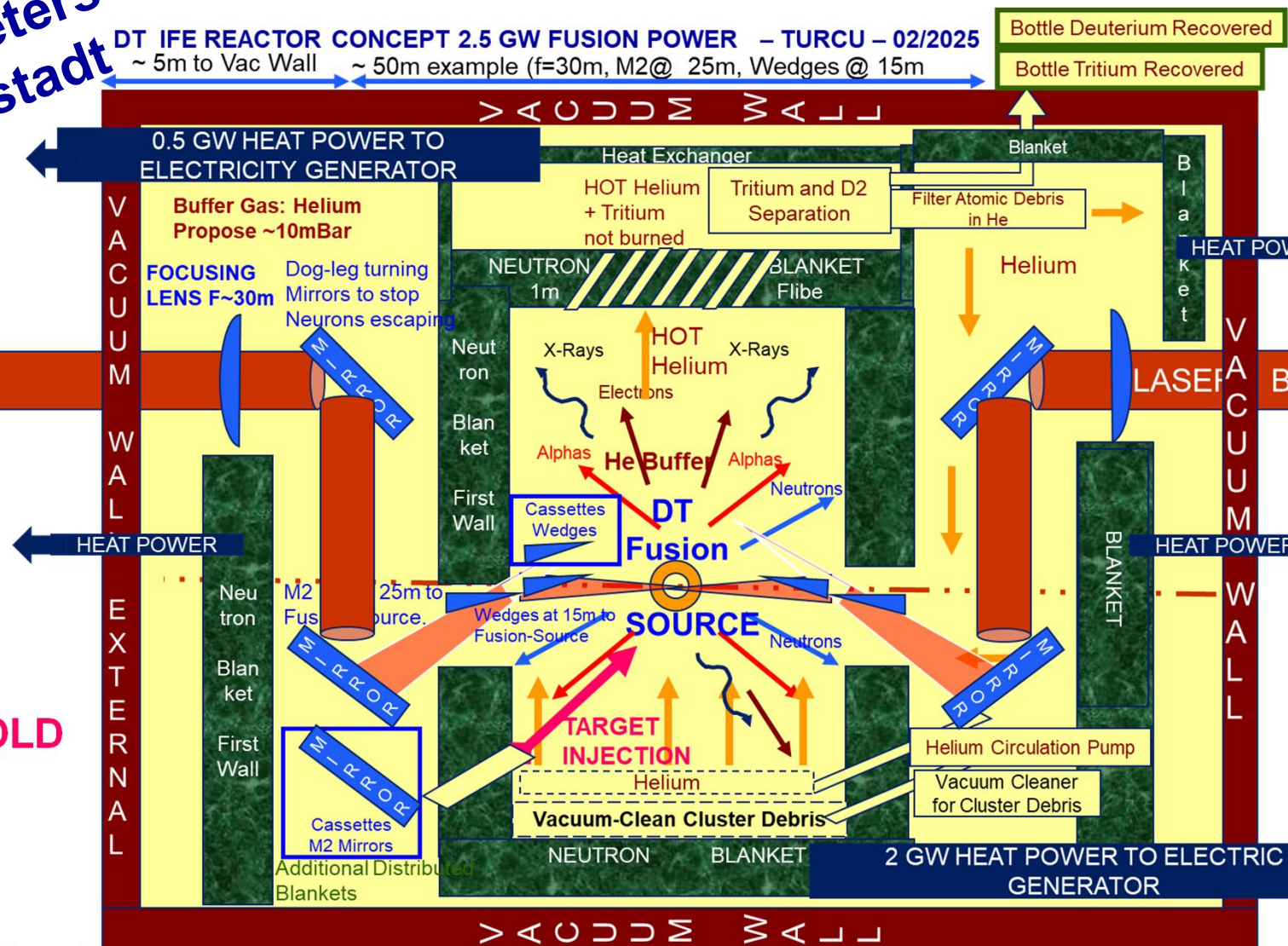
08/09/2025

Turku Nuclear Fusion FBT Power Reactor – ivvPBF-
Belgrade 08/09/2025

um and Deuterium~10KeV are trapped in He gas.
and D collect at top of chamber and the hot He.
Heat exchanger extract heat ~20% of Fusion Power, 500MW for Hyper.
He and D is separated from He.

**10% of Fuel can be recovered and
recycled: 125gT3/day.**

ARGET INJECTION through the COLD - Bottom of Reactor Chamber



Extend Concept to Aneutronic Fusion Power Reactors: Ion and X-Ray Radiation instead of Neutron Radiation

10 MeV Neutrons 80% Fusion Power: heat First Wall and
 Heat Power to Electric Generators.

3.5 MeV Alphas 20% of Fusion Power: Heat Buffer gas, heat
 exchanger, Heat to Electric Generators
 50% X-rays

on Boron Fusion and Deuterium-Helium-3 : Preferred Reactions

11.4 MeV Alphas 100% of Fusion Power: Heat Buffer gas,
 heat exchanger, Heat to Electric Generators

DT, Significant Bremsstrahlung emission because of
 neutron with Z=5. Also part of the Alpha Energy heats
 electrons which generate even more Bremsstrahlung.

Example: 50/50% Alpha-Xray emission – **work required:**

**Direct Conversion of Bremsstrahlung Power to
 Electric Power in X-Ray PIN Diodes or 'X-Ray
 Converter Pannels' : Solar X-Ray-Panels for OUR
 Artificial X-Ray-Sun**

fuel	T_i [keV]	$P_{\text{fusion}}/P_{\text{Bremsstrahlung}}$
${}^2_1\text{D}-{}^3_1\text{T}$	50	140
${}^2_1\text{D}-{}^2_1\text{D}$	500	2.9
${}^2_1\text{D}-{}^3_2\text{He}$	100	5.3
${}^3_2\text{He}-{}^3_2\text{He}$	1000	0.72
$\text{p}^+-{}^6_3\text{Li}$	800	0.21
$\text{p}^+-{}^{11}_5\text{B}$	300	0.57

fuel	Z	E_{fus} [MeV]	E_{ch} [MeV]	neutrons
${}^2_1\text{D}-{}^3_1\text{T}$	1	17.6	3.5	1
${}^2_1\text{D}-{}^2_1\text{D}$	1	12.5	4.2	0
${}^2_1\text{D}-{}^3_2\text{He}$	2	18.3	18.3	0
$\text{p}^+-{}^{11}_5\text{B}$	5	8.7	8.7	0

HB11 and DHe3 Fusion Fuels for Aneutronic Fusion Power Reactors:

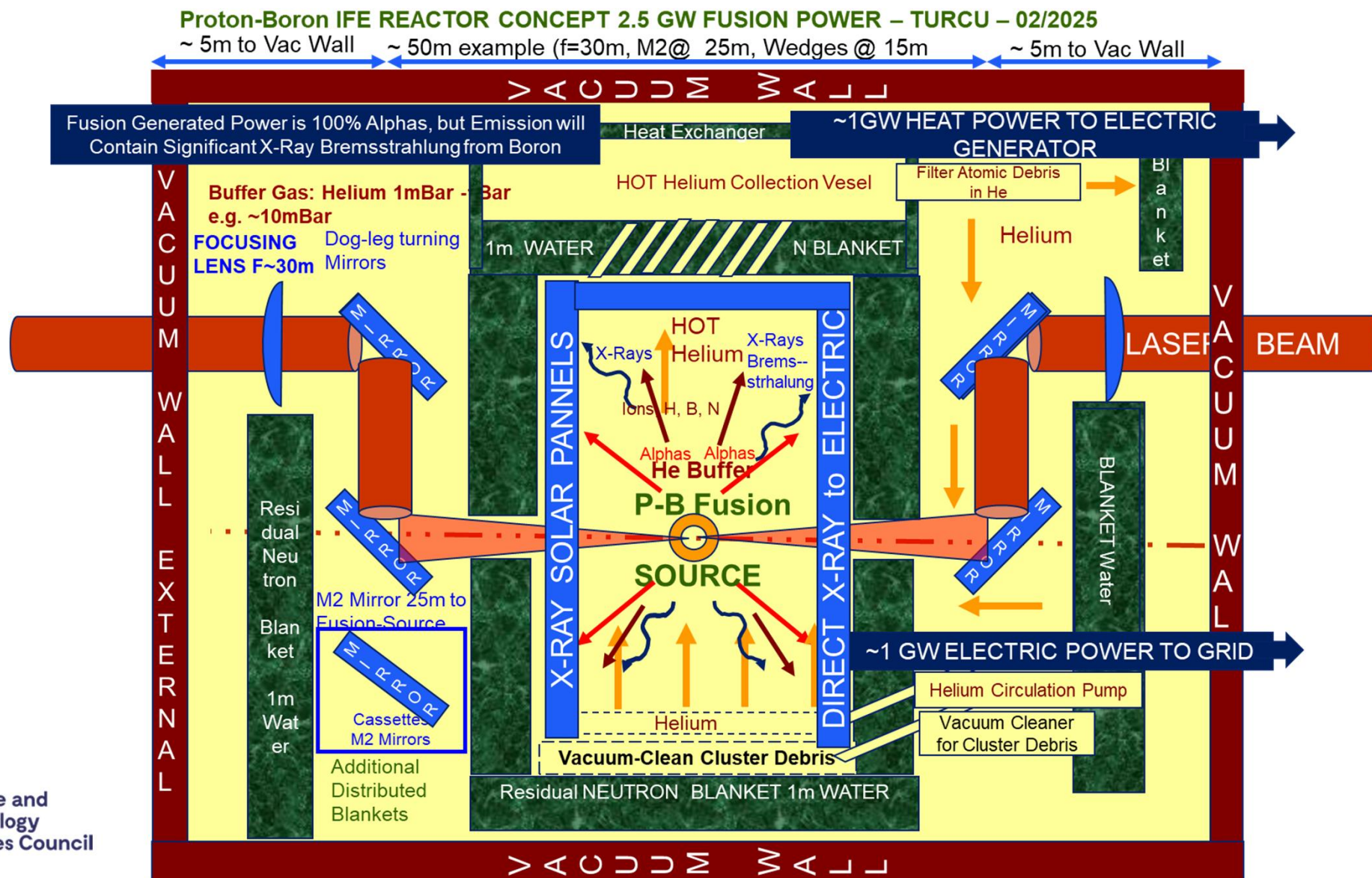
1 Fuel solid at Room temperature, example:
 NH₆, Ammonia Borane NOT Cryogenic, non-Toxic
 2H₆, Di-Borane, LN₂ Cryogenic, Toxic
 -Ray Bremsstrahlung: Large Fraction
 Higher Fusion Temperature than DHe₃
 Higher Fusion Crosssectionn but over narrow Energy Range
 neutron Very Low emission

3 Fuel:
 need to produce He₃ for example from DD Beam Fusion
 cryogenic
 -Ray Bremsstrahlung: Considerable Fraction
 neutron Low emission

fuel	T_i [keV]	$P_{\text{fusion}}/P_{\text{Bremsstrahlung}}$
${}^2_1\text{D}-{}^3_1\text{T}$	50	140
${}^2_1\text{D}-{}^2_1\text{D}$	500	2.9
${}^2_1\text{D}-{}^3_2\text{He}$	100	5.3
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user-IFE Proton-Boron Reactor Concept-example with only two laser beams: Only Residual Neutron Radiation. X-Ray 'Solar Pannels' convert X-rays directly to Electricity. Vacuum Wall is External Wall. Buffer gas in chamber stops ions and Converts Alpha Power to Heat Power.



Buffer Gas Stops 3MeV Alphas and Convert their Energy into Heat. Also stops all 'Ionic debris'

Alpha Range in He at 1atmosphre: $1.5 \times 10^{-3} \text{ cm}^2/\text{g}$ [Williamson et al., CEA-R-3042 (1966)].

range $\sim 9\text{cm}$ at 1000mBar Buffer pressure: $\rho (\text{He atm}) = 1.64 \times 10^{-4} \text{ g/cm}^2$

range $\sim 10\text{m}$ at 10mBar Buffer pressure – assume our IFE Reactor works with 10mBar He buffer.

range is shorter $\sim 1\text{meter}$ if we consider the interaction of Alpha^{+2} with IONIZED He^{+2} Buffer Gas even at 10mBar pressure.

"Snow-Plough Effect" [Marshall L. Ginter and Thomas J. McIlrath, Debris and VUV emission from a laser-produced plasma", APPLIED OPTICS, 5, 885-9 (1988); D. W. Koopman and R. R. Goforth, "Collisional Coupling in Counterstreaming Laser-Produced Plasmas," Phys. Fluids 17, 1560 (1974)]

means most 3MeV Alphas are stopped within $\sim 1\text{meter}$ Radius of Fusion
even in 10mBar of He.

Gas Eliminates Debris Damage: experimental proof

1Bar + Flow: 100W, 100Hz, laser, $>10^{15} \text{ W/cm}^2$;

tape 20um thick [Turcu, J Wiley 1998], work at CLF, UK

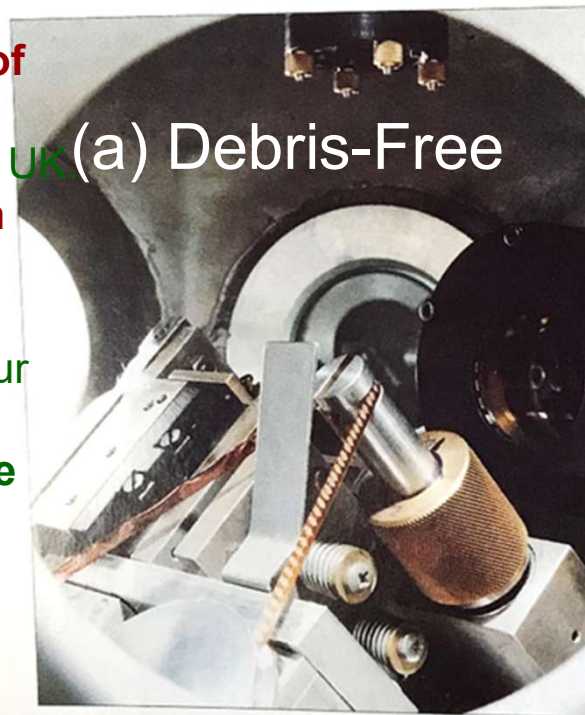
continuous operation as industrial Prototype at JMAR in

lego: 0.3Bar, 300W laser, 300Hz, $>10^{15} \text{ W/cm}^2$

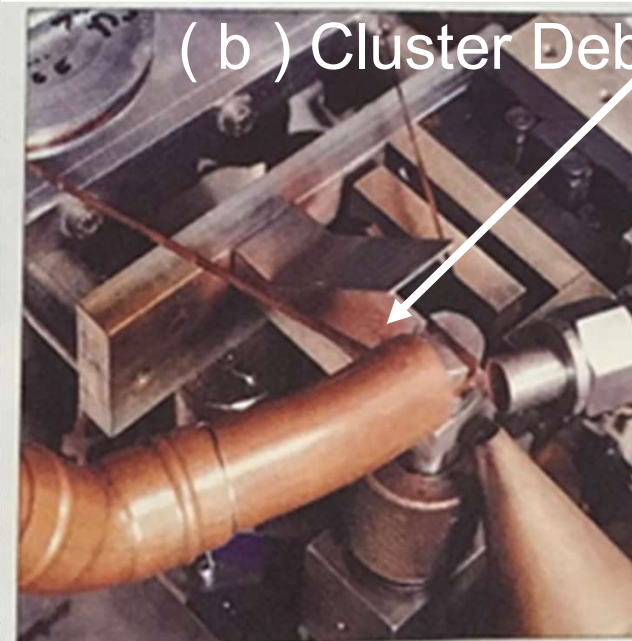
Atomic Debris eliminated by 'Snow-plough' effect

reaction of plasma ions with He^{+2} Buffer Ions. Cu vapour
condensates and deposits in the filter of the flow system.

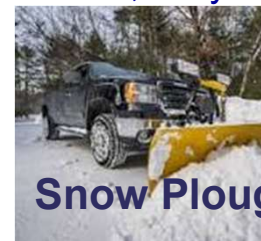
Cluster Debris are heavy and falls at the bottom of the chamber.



(a) Debris-Free



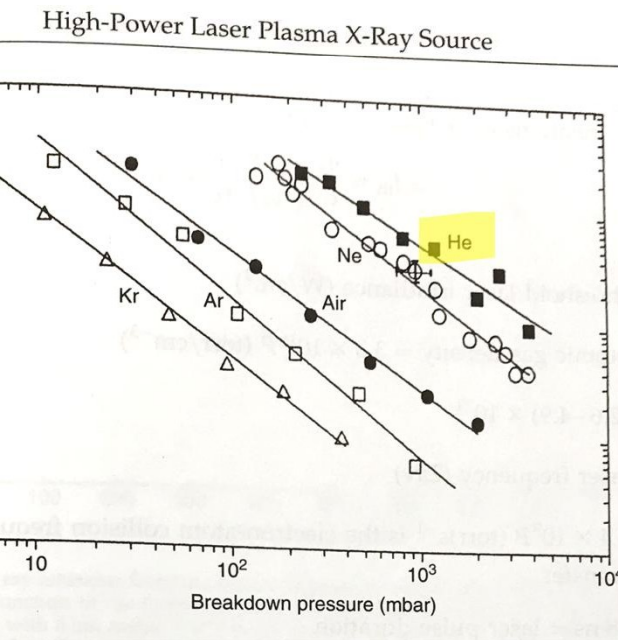
(b) Cluster Debris



Snow Plough

For Gas considerations: He Gas Breakdown Intensity $>10^{14} - 10^{15}$ W/cm² for 25ns UV laser
 0.25um Laser: LPP X-Ray KeV emission unchanged by He Buffer gas to 1Atm

Buffer Pressure and Type and Gas is chosen for the highest
 Breakdown Threshold. X-Ray Source: No X-ray Loss in Buffer Gas
 F: KrF (0.25um) He-1Bar, JMAR YAG (1um) laser, He 0.3Bar



217

218 X-Rays from Laser Plasmas

in the case of the gas breakdown dominated by inverse Bremsstrahlung absorption, the relationship between I_{th} and P is [7]

$$I_{th} \approx \frac{n_a}{c_i} \left(\frac{\omega}{\nu_{ea}} \right)^2 \frac{1}{\tau_L} \ln(i_B V_F n_a)$$

where

I_{th} = threshold laser irradiance (W/cm²)

n_a = atomic gas density = $3.3 \times 10^{16} P$ (torr/cm⁻³)

$c_i = (2.6-4.9) \times 10^{23}$

ω = laser frequency ($2\pi\nu$)

$\nu_{ea} = 2.4 \times 10^9 P$ (torr)s⁻¹ is the electron-atom collision frequency for momentum transfer

$\tau_L = 18$ ns = laser pulse duration

a) also shows that the helium gas breakdown threshold laser intensity is inversely proportional to the gas pressure (P):

$$I_{th} \approx 6.9 \times 10^{15} P(\text{mbar})^{-1}$$

good agreement with an inverse Bremsstrahlung absorption process for breakdown. Morgan *et al.* [6] have shown that for short laser pulses,

$\beta = n_e/n_a \approx 10^{-3}$ = degree of ionization required for breakdown initiation

r_F = about $10 \mu\text{m}^3$ in the experiment described above

In addition to the breakdown threshold irradiance being inversely proportional to the gas pressure, it is also inversely proportional to the laser pulse duration. This implies that when the pulse duration is reduced from 18 ns to, say, 5 ps, the breakdown threshold for helium gas at atmospheric pressure should increase from 5×10^{12} to 1.8×10^{16} W/cm². This is higher than the irradiance used for the picosecond KrF laser system (Section 6.2) that generates the plasma source (Section 7.8).

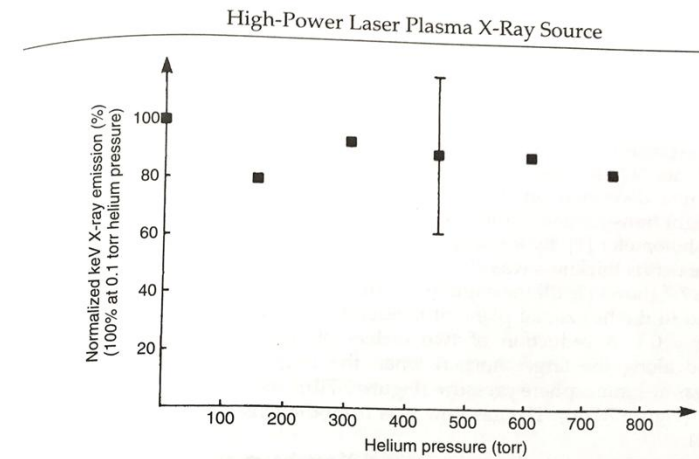


Figure 7.6 X-ray emission from the copper target (Cu L-shell) irradiated by the laser system, as a function of the helium pressure in the target chamber. The signal from the diode (filtered with 6 μm mylar + 60 nm Al) is compensated for the helium absorption and normalized to the signal recorded when the target chamber is in vacuum. The estimated shot-to-shot error is shown by the error bar. (Reproduced from Ref. 1)

the paragraph above. This result is important, since it allows a laser to be used in the X-ray chamber. This makes it possible to:

- Stop target debris from reaching the lens and the X-ray beamline.
- Increase the X-ray source average power by increasing the repetition rate of the laser, as the gaseous debris from the target accumulated on the target can now be removed by flowing helium (Figure 7.2). It was found that a 20 l atm/min cm² helium flow rate allowed a repetition rate of 10 Hz [2]. When the repetition rate of the '20 ns KrF laser system' (Section 7.4) is increased above this value, the X-ray emission stops and a 'searchlight effect' appears; i.e. the laser beam propagates through the target is absorbed and scattered by the atomic debris, giving the appearance of a searchlight focused in fog. The effect disappears when the helium flow rate is increased.
- Use a thin X-ray window in the X-ray beamline, as there is no difference between the X-ray chamber and the external atmosphere.

7.3 Reduction of target debris by the buffer gas

7.3.1 Atomic debris

The debris reduction obtained by filling the target chamber with helium compared with operation in a vacuum. The deposition rate of quartz plates placed 77 mm from the plasma source was measured.

-I-N Silicon/Ge/Diamond X-Ray Diodes, XRD, Convert LPP X-rays and UV Radiation to Electric Power, even $\geq 100\text{keV}$ Bremsstrahlung Photons

RD:

efficiency of 100%
 responds to a sensitivity of
 $7 \text{ C/J} = e\text{-charge} / \text{gap-Si} =$
 $\exp(-19 \text{ C} / 3.7\text{eV})$

Diodes can work in pulse mode
 (PP) and in continuous mode
 (kamaks)

Diode materials: Si, Ge,
 Diamond, etc.

Normally used as X-ray
 detectors with area of mm^2 to
 2 cm^2 .

We could build a matrix of
 such diodes to cover full solid
 angles around Laser-Fusion
 plasma.

intensifier, on the phosphor plate by taking an image with a Polaroid or CCD camera. This deflection is proportional to the emission time with respect to a zero-time fiducial. Figure 3.6(b) shows a view of the Kentech [5] re-entrant streak camera, operating in the vacuum of the X-ray chamber with no X-ray window.

3.3 The p-i-n X-Ray Diode

The calibrated detectors used in most of this work are p-i-n silicon semiconductor X-ray diodes (PIN-XRD) manufactured by the Quantrix Corporation [6]. In comparison with vacuum X-ray diodes, the semiconductor X-ray diodes do not require vacuum operation and the sensitivity of the active region does not degrade in time. Thus they provide reliable, calibrated measurements. Their sensitivity is restricted to X-ray photon energies above 0.3 keV, and usually above 1 keV. However, ultra-thin window diodes are manufactured that offer good sensitivity to lower photon energies.

As nearly all the energy of the X-ray photon is used to generate many electron-hole pairs, the sensitivity of the PIN-XRD is some orders of magnitude higher than that of vacuum X-ray diodes. Figure 3.7 is a schematic representation and internal field profile of a semiconductor X-ray detector [7]. The X-ray interaction depicted is the Compton effect, which occurs at medium X-ray energies. In the case of soft X-rays, photoelectrons and Auger electrons are generated in the semiconductor material. The active region, D, of the detector is the intrinsic silicon region. As this type of detector is the main calibrated X-ray

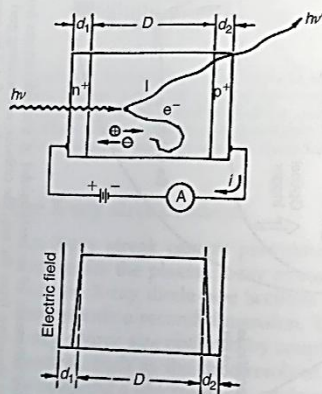


Figure 3.7 Schematic representation and internal field profile of a semiconductor X-ray detector. The X-ray interaction pictured is the Compton effect which occurs at medium X-ray energies. In the case of soft X-rays only electrons are generated (photoelectrons and Auger electrons). (From Ref. 7)

Interaction of Soft X-Rays with Matter: Particle Behaviour

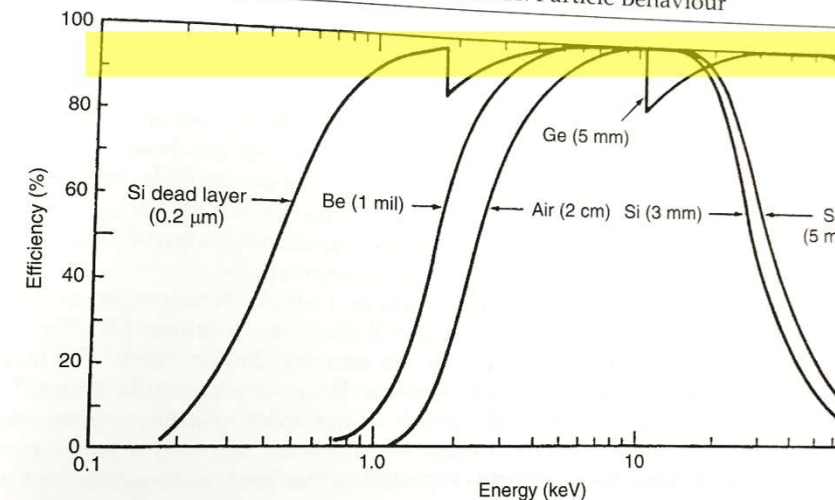


Figure 3.9 Detection efficiency of semiconductor crystals as a function of X-ray photon energy. The thickness of the dead layer of silicon crystals limits the efficiency at low photon energies; the thickness of the detector crystal limits the detection of high-energy photons; and absorption of X-rays by windows and environmental gases, like air, also limit the efficiency at low photon energies. (From X-Ray Data Booklet [2])

Life-Time of X-Ray-Panel Converter at Large Distance to Fusion Source

XRD (X-ray Diodes) convert efficiently X-ray energy directly into electric current.

Life-time of PIN XRD in GW X-Ray Flux, $\sim 100\text{KeV}$ photons?

because proposed First Wall Distance to Fusion Source is Large

X-Ray Flux on XRD Panel at Large Distance from Fusion Source:

10m, Flux $\sim 250\text{ Watt-X-Ray/cm}^2$

10m, Flux $\sim 65\text{ Watt-X-Ray/cm}^2$

Long-term measurements of SXUV100 diode

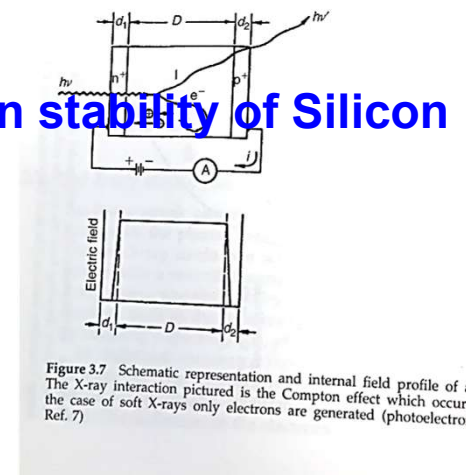
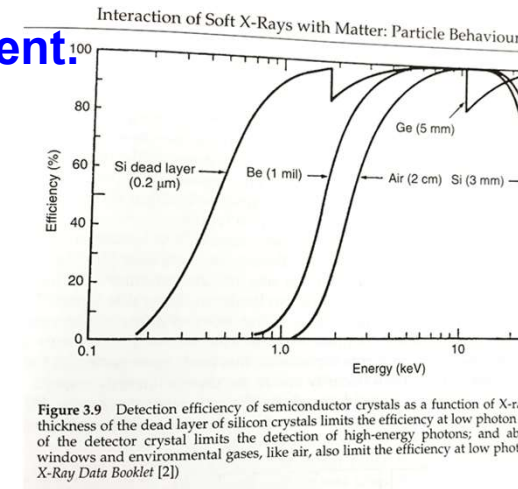
PERCENTAGE CHANGE in X-Ray, 100eV, Sensitivity after large dose on

SXUV100 diode: 160 kJ/cm^2 .

Protect XRD with more EUV protection: window of metal-silicide instead of SiO_2 .

See Korde et. al., Metrologia, 40, S145-S149 (2003); F. Scholtze et al., "Irradiation stability of Silicon photodiodes for EUV Radiation", Applied Optics, 42, 5621-5626 (2003).

Work on Hardening XRD for Space Missions is Ongoing.



Conclusions

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7. Replace Neutron Radiation Converter Wall with X-Ray Radiation Power Converter Panels
8. HB11 and DHe3 Aneutronic Fusion Fuels comparison

Acknowledgements

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Хвала !
Hvala vam
Thank You!